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### Memorandum

To: Chris Lichens - USEPA

From: Dave Chamberlin - CDM

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Date: February 5, 2007

Subject: Technical Memorandum

Soil Vapor Extraction Pilot Test Initial Findings

Omega Chemical Superfund Site 10500-37240-T2.OSS.SVEOP

10500-5.2.3

#### 1.0 Introduction

Camp Dresser & McKee Inc. (CDM) has prepared this Technical Memorandum (TM) on behalf of the Omega Chemical Site Potentially Responsible Party (PRP) Organized Group (OPOG) to present the findings of soil vapor extraction (SVE) pilot testing at the Omega Chemical Superfund Site (Site). This document has been prepared in accordance with the Statement of Work (SOW) in Consent Decree (CD) No. 00-12471 between the United States Environmental Protection Agency (EPA) and OPOG, which required OPOG to implement a vadose zone remedial investigation/feasibility study (RI/FS) for contaminant releases on, at, or emanating from the Site. The CD was lodged on November 24, 2000 and entered into the US District Court on February 28, 2001.

The Site consists of the former Omega Chemical Corporation property encompassing approximately one acre located at 12504 and 12512 East Whittier Blvd. and the Phase 1a Area. As defined in the CD and illustrated on Figure 1-1, the Phase 1a Area is the area of soil and groundwater contamination associated with the Omega property and extending downgradient approximately 100 feet southwest of Putnam Street.

The pilot test was conducted to collect data to confirm the feasibility of SVE and to assist in the design and implementation of a potential full-scale SVE system at the Site, if appropriate. The primary volatile organic compounds (VOCs) at the Site and adjacent parcels are



tetrachloroethene (PCE), trichloroethene (TCE), 1,1-dichloroethene (1,1-DCE), Freon 113, and Freon 11.

The pilot test was performed according to the methods described in Soil Vapor Extraction Pilot Test Work Plan (CDM, August 4, 2006) and consisted of two types of tests: step testing and a multi-week pilot test. The step testing was performed to evaluate the relationship between applied vacuum at the SVE wells and 1) the resulting vapor flows; and 2) the resulting vacuum distributions in the subsurface around the wells. The multi-week test provided design information for potential implementation of the SVE technology once near-equilibrium conditions had been established by operating the SVE system for several weeks. In addition, extended operation provided data concerning the mass of contaminants in the vicinity of the test wells.

### 2.0 Objectives

The overall objectives of the SVE pilot test were to collect additional data which will be used in the selection, design, and implementation of the overall on-site soils remedy for the Site. Specifically, the collected data will aid in selecting the most appropriate SVE design parameters for a potential full-scale system at the Site.

It should be noted that, during the recently completed remedial investigation, an important lithologic layer starting at an approximate depth of 30 feet bgs (hereinafter referred to as the 30 foot clay unit) was noted in borings advanced at the Site and in the vicinity. The 30 foot clay unit is between 3.5 to 11 feet thick, and the top of the unit slopes to the west and southwest (additional discussion is provided in Section 2.4.4 of the RI report). In addition, as discussed in Section 5 of the RI report, the unit appears to be an important factor in contaminant fate and transport at the Site.

Specific objectives for this pilot test included:

- Confirm the feasibility of SVE for site conditions above the 30 foot clay unit identified during implementation of the recently completed remedial investigation.
- Confirm the ability of vapor phase granular activated carbon (GAC) to treat extracted vapors to appropriate discharge limits.
- Estimate the contaminant mass removal rate in extracted vapors to size and select the treatment systems for a potential full-scale system and to evaluate air discharge permit issues.



- Estimate the achievable SVE treatment zone sizes for the interval above the 30 foot clay unit to serve as a basis to select well spacing and construction.
- Provide VOC mass removal data from SVE wells screened in two intervals to help in determining the VOC vertical distribution in the vadose zone above the 30 foot clay unit.

#### **Deviations from Work Plan**

The following items were changes from the methods described in the test work plan:

- The work plan called for testing of condensation-based vapor treatment; however, the GAC performed very well and there are concerns regarding the availability of this technology at the scale that would be needed for a full-scale system. Specifically, the manufacturer of this technology currently provides only 100 cubic feet per minute (cfm) units that can be run in series. Such an arrangement for a full-scale system that would need to treat thousands of cfm would be impractical. Therefore, this technology was not tested.
- The work plan called for collection of transient vacuum readings during a minimum
  of two of the step tests to allow for calculation of intrinsic permeability of the soils.
  These readings were inadvertently not collected; however, the vacuum distribution
  data that were collected provided a more technically sound basis on which to design
  the well spacing for a full-scale system. For completeness, the transient data will be
  collected as part of the proposed extended testing, if approved.

#### 3.0 SVE Well Installation

Between September 7 and 11, 2006, 10 SVE/monitoring wells were installed on the Site for pilot testing purposes. SVE well locations are shown in Figure 3-1. The SVE wells were installed using 10-inch diameter hollow stem augers and constructed of 4-inch diameter Schedule 40 PVC. Each borehole was continuously sampled using a split spoon sampler to document the soil profile at each location. Five shallow-depth SVE wells (VE-1S to VE-5S) were screened from 12 to 22 feet with 20-slot (0.020-inch opening) perforated PVC casing. The total depth of the shallow-depth SVE wells was approximately 23 feet bgs. Five medium-depth SVE wells (VE-1M to VE-5M) targeted the thin sand layer that exists above the 30-foot clay unit. The total depth of these SVE/monitoring wells was approximately 36 feet, with a screened interval over the lower 10 feet which also used 20-slot perforated PVC casing. # 3 Monterey sand was used for filter pack around the well screens. Hydrated medium-sized bentonite chips (approximately 3 feet thick) were placed in the annulus above the filter pack. The rest of the annulus was backfilled with Portland cement (with 5% bentonite added) grout to the ground surface. Surfaces at each location were completed with a flush-grade, water-



tight, traffic-rated surface completions. Table 3-1 summarizes the SVE well construction details.

The lithology encountered during well installation was continuously logged from the surface to the final depth according to the Unified Soil Classification System. The boring logs are presented in Appendix A. Field activities were performed in accordance with CDM's Standard Field Procedures Manual and CDM Health and Safety Plan (HASP) for the Omega site. A CDM geologist was present during all of these Site activities.

During drilling and completion of the soil borings, headspace measurements using a MiniRAE photoionization detector (PID) were performed on soil samples at approximate 5-foot intervals. Recorded measurements ranged from 0.0 to 47 parts per million by volume (ppmv). In general, PID soil head space readings recorded during the drilling were above background levels.

### 4.0 Equipment Setup

This section summarizes the equipment used during the SVE pilot testing.

#### **SVE System Equipment**

Northstar Environmental Remediation (NER) was subcontracted to furnish, set up, and maintain a mobile SVE system. The SVE system used consisted of one 25 horsepower (HP) oil-sealed liquid ring pump (Dekker VMAX450) capable of extracting up to 200 actual cubic feet per minute (acfm) at a vacuum of 29 inches of mercury (in. Hg). The skid mounted system was also equipped with an air/water separator with a high water level shutoff switch and drain pump, a particulate filter, 240-volt, 3-phase, 60-amp control panel, vacuum and flow gages and other instrumentation as necessary to operate the system. All system piping, hoses, and conduits were installed above ground.

#### **Vapor Treatment**

Soil vapors were treated using two 1,000-pound GAC vessels installed in series to comply with requirements of a South Coast Air Quality Management District (SCAQMD) various-locations vapor treatment permit (Permit No. F78354). Sampling ports were installed at the wellhead and at various locations in the system to monitor and collect system influent and effluent vapor samples. The air discharge from the carbon vessels (effluent), as required by the SCAQMD permit, along with system influent and between the lead and lag GAC vessels were tested using a PID unit calibrated with hexane.



#### Other Equipment Used during Testing

The following additional equipment was used during testing:

- Subsurface pressure at vapor probes and non-operating wells were measured using magnehelic gauges or a digital pressure meter (OMEGA HHP-103).
- Concentrations of VOCs in the influent, effluent, and outlet (between the GAC units) streams were monitored with a MiniRAE 2000 PID unit, (11.7 eV ionization potential) and a PE Photovac Intrinsically Safe Handheld Flame Ionization Detector (FID) unit. The instruments were calibrated to 100 ppmv isobutelyene and hexane, respectively. 1-liter designated Tedlar bags were used to collect soil gas samples for field analysis.
- A WS-7394U Wireless 433 Mhz Weather Station was used to monitor barometric pressure changes.
- 2-inch diameter (25 to 125 acfm flow range) and 3-inch diameter (50 to 250 acfm flow range) direct read, in-line flow meters (AMETEK ROTRON) were used to measure flow rates at the wellhead and entering the primary GAC vessel. Some flow rate inconsistencies were noted due to the need to alternate between meters for different steps (due to the range differences).

Field equipments were calibrated in accordance with the manufacture's instructions. Instruments requiring field calibration were checked and adjusted before and after each day of use.

#### 5.0 Pilot Test Procedures and Field Measurements

Between October 17 and November 9, 2006, CDM conducted 15 one-day step tests (10 single-well and five combination-well tests) at the 10 SVE well locations. The SVE system is located in the portion of the Site formerly occupied by 3 Kings Construction. Appendix B contains a detailed discussion of pilot test procedures and results. The field data collected during the pilot test are summarized in Tables 5-1 through 5-3. Graphs illustrating vacuum measurements collected at each well versus the applied vacuum at each step are also provided in Appendix B, Figures B-1 through B-10.

### 6.0 Analytical Sampling

Soil vapor samples were collected from the system influent, between the GAC canisters (outlet) and system discharge point (effluent) and analyzed for VOCs in accordance with EPA Method No. TO-15. Soil vapor samples were submitted to SunStar Laboratories, Inc (SunStar), a State-certified environmental laboratory located in Tustin, California. The air samples were



collected by using 1000 cubic centimeter (cc) silonite-coated steel canisters provided by SunStar. Table 6-1 summarizes the soil vapor analytical results. The laboratory analytical reports are provided as electronic pdf files on the compact disc in Appendix C.

#### 7.0 Evaluation of Pilot Test Results

This section presents an interpretation of the test results with regard to the test objectives.

#### Radius of Influence

Typical pressure distributions (both plan view and in cross section) that were measured during testing are included in Appendix D, Figures D-1 through D-9. The achievable radius of influence (ROI) during the testing was typically greater than 75 feet. This uses a ROI that is defined by at least 0.1 in.  $H_2O$  vacuum. Such an ROI was typically achievable by applying approximately 10 in.  $H_3$  to the both shallow and medium wells. The corresponding vapor extraction rate ranged between 50 and 70 standard cubic feet per minute (scfm) for the shallow wells and 68 and 103 scfm for the medium wells (Figure D-2).

The vacuum distribution data indicate that vacuum was induced in the medium soil depths during operation of the shallow wells and vice versa. This indicates that the soils are sufficiently and uniformly permeable to allow the entire 30-foot interval of the vadose zone above the 30 foot clay unit to be remediated by SVE wells screened over one long interval (as opposed to the two screen intervals used for the test).

#### **VOC Mass Removal Rates**

The analytical results indicated that the VOCs most commonly detected in the soil vapor samples were PCE, TCE, 1,1- DCE, Freon 11, and Freon 113. Distributions of the VOC concentrations are illustrated for both shallow and medium SVE wells and are included in Appendix E (Figures E-1 through E-3).

These data can be used to determine breakthrough times for each VOC which can in turn be used as a basis to design full-scale GAC treatment units and estimate breakthrough times for such a system, as appropriate.

The VOC mass removal rate for the system was estimated by multiplying the linearly interpolated daily extraction flow rate by the linearly interpolated VOC concentrations of the soil gas samples. Analytical results of the system influent were used to calculate VOC mass removal rates (Figure 7-1). The estimated VOC mass removal rates and cumulative mass removal are presented in the operations summary (Table 7-1) and illustrated in Figures 7-2 and 7-3.



Between October 17, and November 22, 2006, approximately 415 pounds of VOCs were estimated to have been removed from the Site. In general, VOC mass removal rates of approximately 35 pounds per day (lbs/day) were achievable from each well, although the rates increased at those wells that were closer to the Star City Auto Body building.

#### Vapor Treatment

The soil vapor analytical data collected at the system influent, in-between carbon units, and at the effluent port of the GAC units indicated that the GAC was capable of removing all VOCs in the extracted vapors (Table 6-1). Based upon the recorded flow rates, it is estimated that approximately 7.2 million cubic feet of soil vapor were extracted and treated during this pilot test.

#### 8.0 Conclusions

The following are the main conclusions of the pilot test performed as of the writing of this TM:

- SVE is a feasible technology for the vadose zone above the 30 foot clay unit.
- A ROI of at least 75 feet could be achieved at the shallow wells at an applied vacuum of approximately 10 inches of Hg. This resulted in a vapor extraction flow of approximately 50 to 70 scfm.
- A ROI of at least 75 feet could be achieved at the medium wells at an applied vacuum of approximately 10 inches of Hg. This resulted in a vapor extraction flow of approximately 68 to 103 scfm.
- VOC mass removal rates ranged from 2 to 84 pounds per day, depending on the SVE well operated. A total of 415 lbs of VOCs were removed during this pilot test. The results indicated that there is generally more VOC mass in the medium depth soils compared to the shallow depth soils.
- The GAC treatment units were capable of removing the VOCs found in the extracted soil vapors. The analyses of the samples that were collected at the GAC units provided a basis to evaluate and design GAC treatment for a potential full-scale SVE system, if appropriate.
- The vacuum distributions measured during testing indicated that single depth wells could be used to remediate soils above the 30 foot clay unit (as opposed to the dual depth wells that were used in this testing).



### 9.0 Recommendations for Proposed Additional Testing

In order to collect data that may be critical to evaluation and comparison of different SVE alternatives in the Feasibility Study, it is proposed that the SVE pilot testing be expanded to gather more data concerning the heterogeneity of the vadose zone in the source area and the peak and constancy of the VOC concentrations that may be encountered with a full-scale system. The site conceptual model indicates that the area of highest VOC concentrations in the upper vadose zone is likely to be between Star City Auto Body and the Medlin building located in the northwestern quadrant of the Site. The pilot test should be expanded by installing four new wells in this area that should be screened from 10 to 30 feet bgs. The benefits of this expansion would be to 1) verify the conclusion that two screened intervals are not required for the soils above the 30-foot clay unit, 2) determine the heterogeneity of the soils throughout the site, 3) determine the peak VOC concentration, and (4) determine the impact of removal on the total VOC mass in the vadose zone. As before, these wells would be able to be used as SVE wells or as monitoring wells to collect vacuum readings. Two of these proposed wells would be located to the north of Star City, one behind the loading dock at the back of Star City, and one further to the west on the Terra Pave property, as shown on Figure 9-1.

Information gained from operating these additional wells will be used to assess the cost effectiveness of using GAC for vapor treatment for a full-scale system. While the existing test data confirmed that GAC is feasible for vapor treatment at the Site, uncertainty about the mass of VOCs in the targeted soils precludes identifying which vapor treatment technology is most cost effective. For example, if the VOC mass in the proposed test expansion area is very high, then a technology such as the condensation based treatment would likely be more cost effective than GAC. To address this uncertainty, it is proposed to operate the new wells for a minimum of 2 months to determine how quickly the VOC concentrations in the extracted vapors decrease, as this will be relative to the mass of VOCs present within the ROI of the wells. In addition, the proposed well spacing will confirm the earlier results that indicate a design ROI of 75 feet is achievable throughout the Site, and provide important information on the efficacy of SVE in other areas of the Site.

The data collected during the pilot test demonstrate that the SVE system is highly effective in removing VOC contaminant mass from the subsurface, and thereby reducing in-situ soil vapor concentrations. Because migration of these shallow soil vapors to indoor air represent the only potentially completed exposure pathway at the Site, continued reductions in mass and vapor concentrations can only have a beneficial impact to the site. In light of this significant beneficial value, and in the absence of any disadvantage to continued operation, it is strongly recommended that the pilot-scale SVE system continue to operate until it is no longer beneficial or a full-scale remedy can be put in place.

## CDM

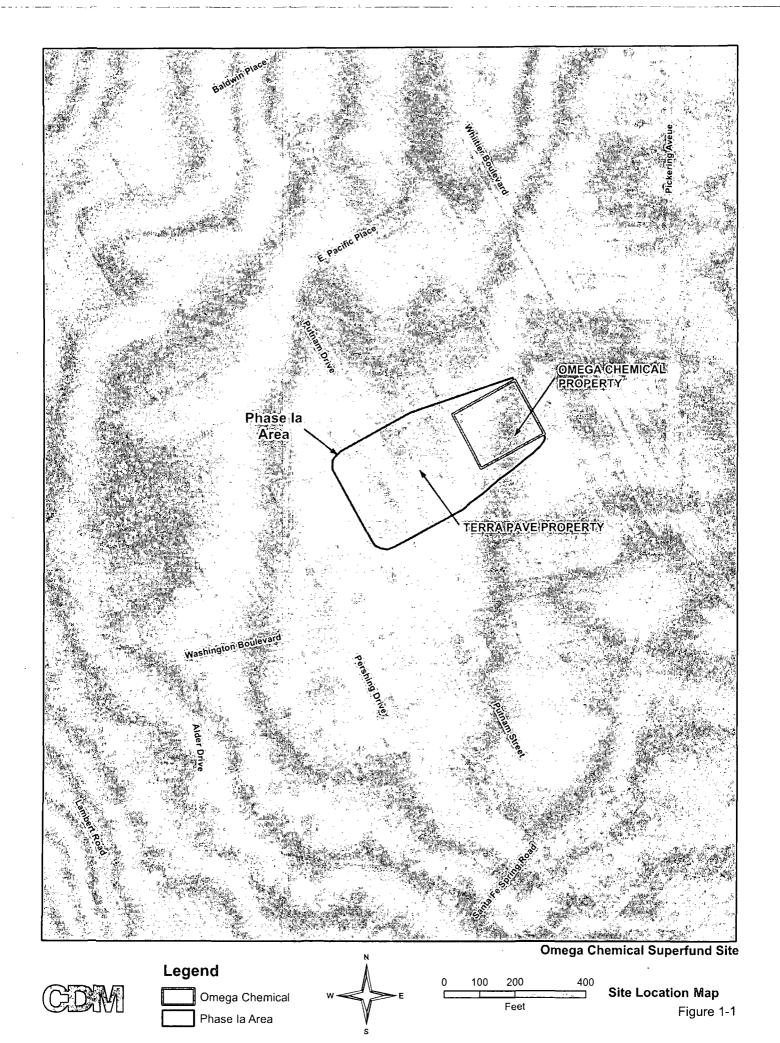
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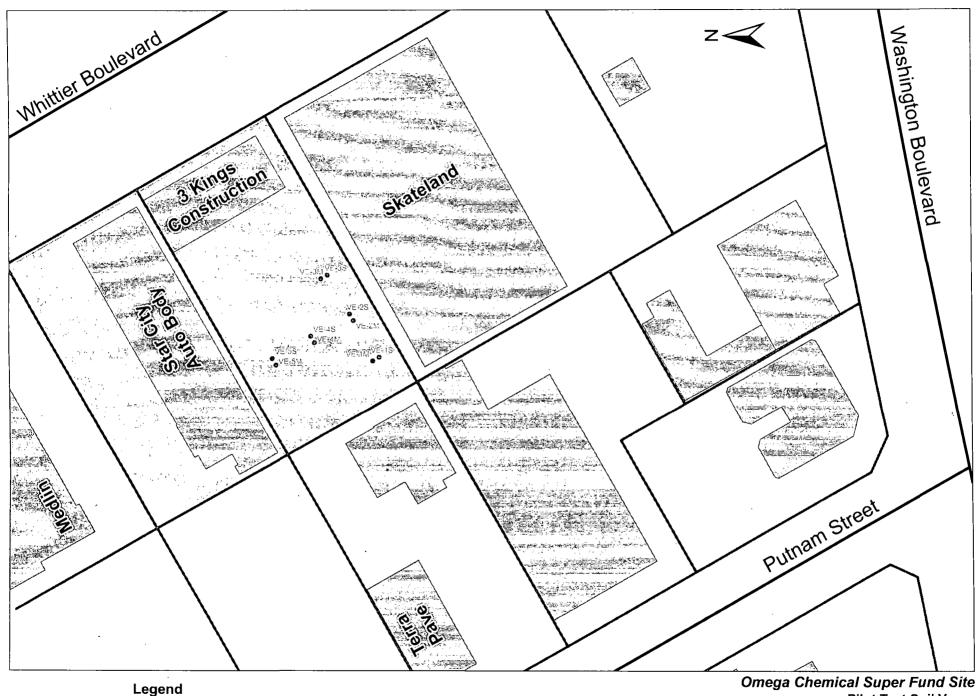
## References

CDM, 2006. Soil Vapor Extraction Pilot Test Work Plan, August 4.

CDM, 2007. Draft Human Health Risk Assessment for On-Site Soils, January 19.

CDM, 2007. Draft On-Site Soils Remedial Investigation Report, January 19.





**CDM** 

Property Boundary
Road Center

Omega Chemical Superfund Site 

Building

Soil Vapor Extraction Well



hemical Super Fund Site
Pilot Test Soil Vapor
Extraction Well Location
Figure 3-1

Figure 7-1
Omega Chemical Superfund Site
Pilot SVE System Analytical Influent Results

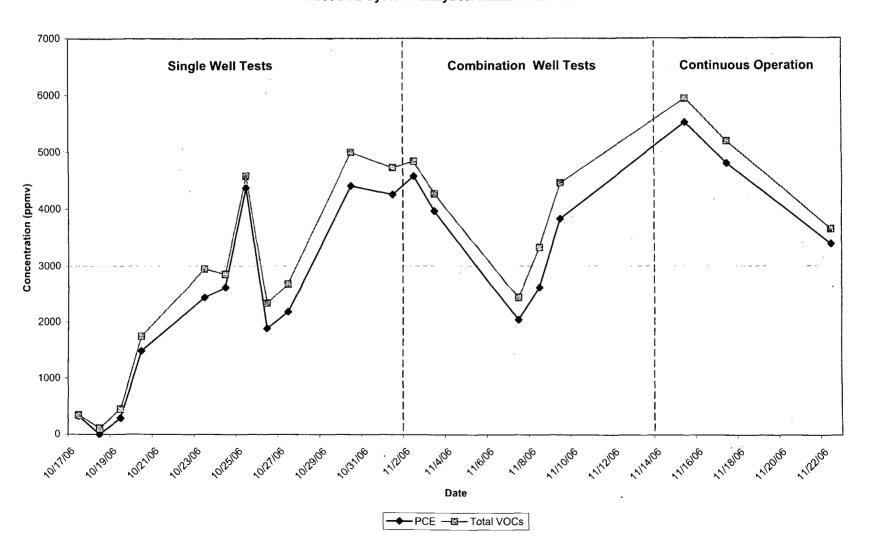


Figure 7-2
Omega Chemical Superfund Site - SVE Pilot Test
Estimated VOC Mass Removal Rates

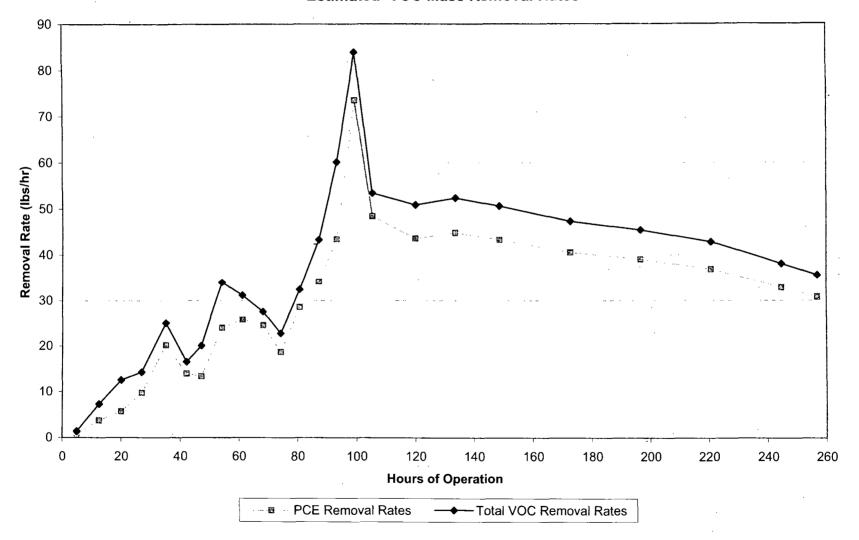
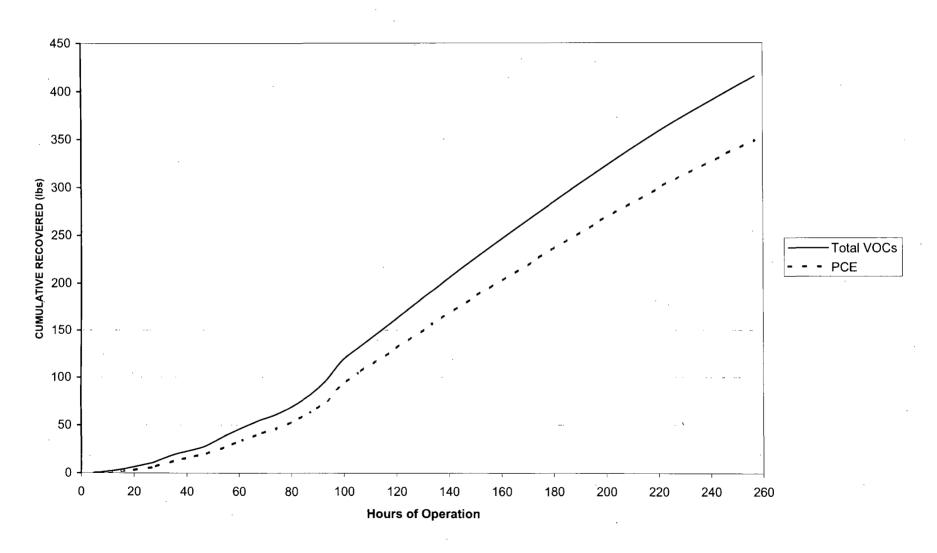
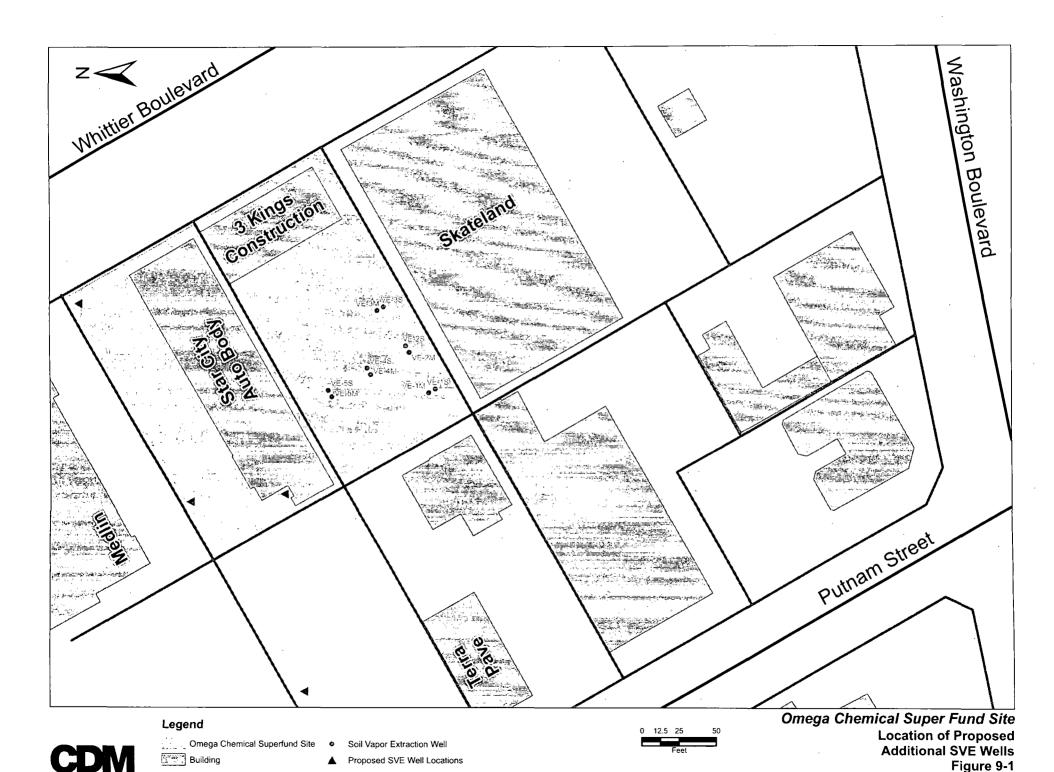


Figure 7-3
Omega Chemical Superfund Site - SVE Pilot Test
Cumulative Mass Removal



1 of 1





--- Property Boundary

Table 3-1
SVE Well Construction Details
Omega Chemical Superfund Site

Well ID	Total Drilled Depth (feet)	Screened Interval (feet bgs)	Filter Pack Interval (feet bgs)	Bentonite Seal Interval (feet bgs)	Date Drilled
VE-1S	23	12.5 - 22.5	10 - 23	7 - 10	9/7/2006
VE-1M	36.5	26 - 36	24 - 36.5	21 - 24	9/8/2006
VE-2S	23	12 - 22	10 - 23	7 - 10	9/8/2006
VE-2M	36.5	26 - 36	23.8 - 36.5	21 - 23.8	9/11/2006
VE-3S	23	12.5 - 22.5	9.8 - 23	6.8 - 9.8	9/7/2006
VE-3M	36.5	26 - 36	24 - 36.5	21 - 24	9/7/2006
VE-4S	22.5	12 - 22	9.5 - 22.5	7 - 9.5	9/8/2006
VE-4M	36.5	26 - 36	24 - 36.5	21 - 24	9/8/2006
VE-5S	23	12 - 22	9.9 - 23	7 - 9.9	9/11/2006
VE-5M	36.5	26 - 36	24 - 36.5	21 - 24	9/11/2006

Note:

bgs: below ground surface

Table 5-1 Omega Chemical Superfund Site SVE Pilot Test Single Well Tests Summary

Active Wellhead		Wellhead Vacuum (in. Hg)	Flow Rate (ACFM)	Flow Rate (SCFM)	Liquid Ring Pump Vacuum (in. Hg)	Start Time	End Time	Step Duration (min.)	Influent PID (ppmv)	Influent FID (ppmv)
	Step 1*	10	96	63	25	8:10	9:00	50	76	68.8
VE-1S	Step 2	15	100	47	26	11:01	13:50	169	0.9	70.6
	Step 3	17	125	52	22	13:50	16:15	145	5.3	71
	Step 1	10	85	55	26	8:42	11:04	142	78	363.4
VE-2S	Step 2	13	120	65	25	11:04	13:42	158	85	386.7
	Step 3*	16	120	55	22	13:42	16:16	154	76	393
	Step 1	10	80	50	26	8:38	11:16	158	159	590
VE-3S	Step 2	13	120	64	24	11:16	13:32	136	160	603
	Step 3*	16	128	58	22	13:32	16:05	153	160	581
	Step 1	10	84	54	26	8:20	10:35	135	135	851
VE-4S	Step 2*	14	105	54	24	10:35	13:05	150	142	741
	Step 3*	15.5	130	61	22	13:05	15:25	140	136	679
	Step 1*	8	80	57	26	8:10	10:43	153	289	717
VE-5\$	Step 2*	10	108	70	23	11:52	14:08	136	341	871
	Step 3*	13	117 64 20 14:08 16:23	135	325	988				
	Step 1	10	105	68	23	8:20	10:31	131	119	228
VE-1M	Step 2	12	150	87	21	10:31	13:02	151	155	376
	Step 3	13	170	93	19.5	13:02	15:30	148	189	434
VE-2M	Step 1	9	140	97	21	8:40	11:00	140	165	446
▼ L-ZIVI	Step 2	10	160	103	20	11:00	13:25	145	221	544
	Step 1	6	83	64	24	7:45	10:00	135	403	714
VE-3M	Step 2	10	120	76	20.5	10:00	12:15	135	352	814
	Step 3	12	150	86	18	12:15	14:26	131	341	797
	Step 1	6	85	65	21	8:05	10:33	148	280	531
VE-4M	Step 2	10	110	70	17	10:33	12:50	137	318	675
	Step 3	12	145	82	18	12:50	15:00	130	390	979
	Step 1	6	75	59	26	7:45	9:52	127	378	545
VE-5M	Step 2	9	120	81	18	9:52	12:10	138	487	896
	Step 3	10	105	68	17	12:10	14:26	136	506	955

Notes in Hg ACFM inches of mercury actual cubic feet per minute SCFM standard cubic feet per minute

in. H2O

ppmv

inches of water
parts per million by volume
Data collected during Single Well Data Gap Step Tests

Table 5-2 Omega Chemical Superfund Site SVE Pilot Test Combination Well Tests Summary

Well ID	Wellhead Vacuum (in. Hg)	Flow Rate (ACFM)	Flow Rate (SCFM)	Liquid Ring Pump Vacuum (in. Hg)	Start Time	End time	Trial Duration (min.)	Influent PID (ppmv)	Influent FID (ppmv)
VE-1S	9.2	123	82	17.9	8:30	14:55	385	291	298
VE-1M	4.8	119	96	17.9	3.30	3	303	291	230
VE-2S	9.4	122	81	17.9	8:30	14:55	385	389	470
VE-2M	2.5	118	104	17.5	0.30	17.5	303	309	470
VE-3S	8.1	124	85	16.9	8:50	14:55	365	423	650
VE-3M	6.1	121	91	10.5	6.30	25	303	423	030
VE-4S	8.9	123	82	17.5	8:35	14:40	365	673	1150
VE-4M	6.2	118	89	17.5	8.33	11.1	303	0/3	1130
VE-5S	6.1	80	61	16.9	8:40	14:55	375	848	821
VE-5M	4	76	63	10.5	0.40	14.55	373	040	021

#### <u>Notes</u>

in. Hg inches of mercury
ACFM actual cubic feet pe

ACFM actual cubic feet per minute
SCFM standard cubic feet per minute

ppmv parts per million by volume

# Table 5-3 Omega Chemical Superfund Site SVE Pilot Test Continuous Operation Summary

Week	Date	VE-2S Vacuum (in. Hg)	VE-2S Flow Rate (SCFM)	VE-2M Vacuum (in. Hg)	VE-2M Flow Rate (SCFM)	Influent (ppmv)	Notes
	11/14/2006						
11/14 - 11/19*	11/15/2006	_ 8	91	1.2	82	672	EPA site visit; system shut down due to breakthrough
	11/17/2006	7.9	85	3.5	96	612	Primary carbon vessel exchanged; system restart
	11/20/2006	7 1	98	3.2	99	560	
11/20 - 11/24	11/21/2006			-	-	550	· ·
	11/22/2006	7	96	3	96	502	System shut down due to breakthrough/holidays
	11/29/2006	7.8	93	3.1	101	439	Primary carbon vessel exchanged; system restart
11/27 - 12/1	11/30/2006	_	-	-	_	486.7	
	12/1/2006	-		-	_	465	System shut down due to weekend
	12/4/2006	-		_		509	System restart
12/4 - 12/8	12/5/2006	6.8	-97	3	94	392	
	12/7/2006			_		250	System shutdown due to possible breakthrough
	12/11/2006	7 2	98	3.1	98	262.9	System restart
12/11 - 12/15	12/12/2006	-		_		272	
	12/13/2006			-		250	System shut down due to breakthrough

Notes in Hg SCFM ppmv

inches of mercury standard cubic feet per minute parts per million by volume Operated through the weekend

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Cr 18	17-00-06	15.7/	OUT.	1/0	10	12	10		10	21	10	17	16	10	23	710	1 4	10	10	10	10	10	10	110	7.0	110	10	10	M	8.1	10	10	17	3.5	10
VE-15	17-On 05	73.43		43.790	1/0	F700	750	/300	4.3	11	27	6.5	32	10	10	/4	10	220	me	**	10	10	10	10	211	10	111	10	22000	76	110		10	7500	10
vt 2s	18 On Of	15.47	EFF	425	10		10	44	10	11	10	37	46	7.1	40	10	10	10	24	10	10	15	10	10	-;-	16		10	130	4.7	71	10	67	24	10
VE 25	10-04-05	15.70	OUT	421	10	<b>54</b>	10	66	1 0	10	10	10	31	10	34	10	1.6	10	# 1	10	10	10	1.0	111	7 U	1.6	10	10	270	43	10	1 0	14	29	10
NC 23	18-04-06	14.44	. 14	237 ***	1-0	• 3000	100	11000	Lu.	16	t U	tu	14	10	5.0	12	21	670	4800		**	14	14	13	10	1 tu	t u	1.0	110000	•	11	900	F600	21000	
VE 35	19-013-05	15 36	CIL	527	10	M2	2.1	*	19	10	10	14	34	6.6	10.	10	10	10		10	10	10	l u	1.0	11	10	14	10	180	••	10	10	12	19	10
VE-19	19-CH1-05	15.41	14	4 16,339	150	**000	940	140000	10	260	10	10	9.0	32	11	34		400	111	17	14	10	10	10	2 u	1.0	10	10	160000	72	15	סוייו	20,000	37000	11
NE-45	70-Oct-06	15 GC	ELL	111 661	10	* 100C	1500	61000	10		10 10	40 V	100	100	100	110	-0 U	1400	#100	10 10	10	400	40.0	90	~C U	90	10	2011	240000	10	10	1100	12000	32000	10 900
VE-NS	73-Oct-06	13.47	eir.	446	10	10	10	***	10	Ve	10	14	49	10	41	10	10	10	14	1.0	10	10	10	10	20	10	10	111	161	500	10	16	14	172	14
VE SS	21-On-06	11.51	OUT	179	110	1,0	1.0	52	10	10	14	14	32	10	28	10	10	10	14	1 0	10	10	10	10	7.0	10	10	1.0	**	iú	iú	10	10	10	10
v€ ss	23-Oct-06	17.52	IN	663.983	7190	49000	1600	77000	NO U	40 U	40 U	50 U	40 U	MU	-0 U	200	<b>40</b> U	3100	780	40.0	*0 U	500	40 U	40 U	40.0	100	10 U	NO U	10000	40.0	63	7190	29000	10 U	*0 U
VC-VS	7 5 Oct 05	16 04	EFF	1 04 1	10	1.0	1.0	100	1.0	44	10	16	43	3.3	24	10	1.0	4.5	10	10	10	10	10	10	4.5	10		10	210	10	1.6	10	×	10	10
ve vs	77 On 46	16 OF	154	472 810	1700	29000	1200	-5000	-0 U	MI U	10 U	40 U	*O U	40 U	40 U	210	<b>~0</b> ∪	2-00	100	50 U	50 U	- U	10 U	40 U	10 U	~P U	*** U	~0 U	P-00000	30 U	10 u	1440	18000	15000	-0 u
VE 14	74-06-04	15.03	Err.	169	10	45	1 4	24	10	10	10	10	22	10	1.	10	1 13	10	10	1.0	10	10	10	I U	7.0	10	1 0	16	140	' U	10	19	22	**	10
VC-14	24-On-46	15.06	14	20/ /00	1/00	11000	1400	12000	-n u	-0 U	Nº U	*0 U	50 U	40 U	-0 u	10 U	wa u	1900	1000	NO 0	<b>40</b> U	50 U	<b>~</b> 0 u	50 U	*0 U	-110	*0 U	*6 U	210000	*C U	-00	. 50 0	1700	4400	-60
ME 74	25-OH OF	1300	CFF	3 936	10	27	1700		10 400	64	10	35	50	69	77 90 U	400 40 U	10	1300	10	10	10	220	140	10	1100	10	150	10	180	10	1200	10	10 .	. 27	10
ME 24	25-0s-06 28-0-1-06	14 07	14	757 940	12	25000	1700	9000	10	-00 U	10	**	-00	*0 u	200	11	10	110	27	10	10	32	*0 u	100	100	40 U	400	10	210000 170	-0 Li	40 U	#20 1.h	7900	14	ίη Cu
CE 100	26-Un-46	14 09	19	/11/951	14	19000	1200	160000	400	100	-0 U	100	NO II	400	2017	10.0	¥C U	10	680	700	50 U	10 u	400	100	200	100	70 U	50.0	450000	43	6.3	2900	2,000	29000	200
VE-16	27 Oct 01	14.00	677	271	2.9	24	7.9	91	111	14	116	7,0	10	-	17	12	10	7.6	41	10	10	7	10	10	-	111	A?		120	10	- 27	7.9	20	70	10
VE 24	27 Oct 69	14.10	14	ESC 260	1200	12000	1200	40000	40.0	400	40 0	NO U	<b>10</b> U	40.0	40.0	230	46.0	3100	110	50.0	70 U	×0 tr	50.0	50 U	40 U	40.0	40 U	50 U	40000	40.0	50 U	1300	21000	7900	40 U
NE AM	77-On 66	14.43	EFF	166	10	*	21	110	10	10	10	10	21	10	15	14	10	10	16	10	10	10	1.0	14	2 tu	10	10	10	740	20	2.2	37	IF.	74	10
VE-14	27-04-06	14.45	19	657 570	1700	2*000	1000	75000	NO U	90 U	Y U	• <b>0</b> u	50 U	10 U	100	1,10	<b>~</b> 0 ∪	7600	1000	~C U	50.0	~0 U	*1 U	NO U	40 U	MI U	10 U	NO.	~10000	SF U	~0 U	1100	22000	11000	40.0
VE 544	10-On OF	14.00	EFF	579	79	75	2.4	21	10	14	16	,	10	١,	12	12	10	**	4.1	1 U	10	2	10	10	14	10	12		120	1.0	47	29	70	20	10
VE-544	10-Ort-08	14 10	14	E90 200	1100	17000	1200	10000	<b>~</b> € U	*0 U	40 U	50 U	-0 U	~0 U	-0 U	210	50 U	3100	710	400	<b>~</b> 0 ∪	<b>~0 U</b>	~: ∪	<b>₩</b> U	*0 U	<b>40</b> U	90 to	50 U	190000	50 U	10 U	מחנו	71000	/800	*0 U
ME NS	01-Nov-06	14 09	OUT	569	2100	27/000	1200	P000	10 900 a	10	10	10	40 u	1 U	1∉ 50 ∪	720	1 U	2500	10	10	18	10	10	10	2 u	14	10	11/	170	3	10	,	22	54	13
VE-16	01 V (4	14 17	- 14	FOP PRO	2150	700	1700	P-000	40.	wit.	46 U		4.0	700	300		ombination H		- >40	10 U	30 n	5F U	*0 u	<b>10</b> U	40 U	400	50 U	500	4700fC	50 U	*6 U	2100	27000	11000	:0 U
VC 15: IV	02-Year CF	11.61		201	10	10	10	12	10	3.6	10	7.5			11	10	1 II	(U	10	114	10	110						10	N					- 13	110
VE-13-114	02 Nov 66	11.75	QUT	1/2	10	10	10	',	114	- ;;	10	47	- 33		23	10	10	10	10	10	10	10	10	10	12	10		10	7	10	1 U	10	10		12
VE 18/11V	27 Nov 66	14.77	- 15	311.500	1300	£200	7.0	36000	50.0	*0 U	400	50 U	100	งกับ	10 U	910	50 U	1 100	3.00	100	100	<b>10</b> U	9011	90 D	M11	100	¥€ U	100	250000	100	9011	50 V	3100	2340	100
VE 25/29	03-Nov-01	14.13	EFF	8/5	10	15	10	49	10	20	14	12	44	24	40	14	10	10	111	10	10	11	11	21	•1	1.9	- 51	10	190	10		19	10	12	10
VE 25/2M	03-New 46	14.34	OUT	200	10	11	10	19	10	11	14	15	17	21	22	10	10	1 0	10	10	16	10	10	10	**	112	24	10	3*	10	25	10	10	29	12
VE 25/74	Q1 New 66	14.36	IN.	410 Fat-	<b>#00</b>	1900	1100	N-100	10 (	No. 11	*0 U	<b>40 U</b>	*0 U	*11 U	*0 U	*0 U	*0 U	1200	1200	~n u	50 U	30 U	50 ti	*0 U	*4 U	10 U	10 U	50 U	.000000	50 U	50 til	1100	FF00	11000	100
VE-384.7M	D/ New C6	14 31	EFF	/12	10	41	10	170	10	4.1	10		140	7.6	100	10	10	,	10	10	. ,	10	10	10	19	1.0	19	10	760	10	10	10	18	46	16
VE-15414	07 Hov-06	14 31	QU*	100*	10	51	10	100	10	7.0	10			2.	64	10	1.0	10	111	10	60	10	10	10	4.3	14	24	10	- 7	4.7	10	10	• •	290	24
VE.35414	Of New CE	14 37	14	621 170	100	2 1000	980	140000	100	40 U	N10	10 u	90.0	20.0	*0 u	<b>40</b> U	40.0	590	440	500	100	50 U	*C U	50.0	×0.0	~00	40 U	*0 U	400000	50 U	**	2800	10(100	23000	400
VE 43549	DA New CIE	14 09	CUT	27.448	* U	48	10	72000	10	10	2011	100	10.0	100	200	10 500	10	10	10	10 10	20	10	90.0	10	20	70	10	10	~~0		50.0	400	400	-400	90.0
VEASIAN	00- TH OF	14 17	IN.	A47 325	3100	1.000	HACO	60D)0	4C U	900	50.0	90 U	*0 U	พาย	100	160	~0 U	2900	2700	10 L	400	10 U	- NO.U	100	50.0	400	500	50 U	1000000	NO U	45	7500	25000	10000	700
VE SS/NW	05 4w 06	14 27	OUT	21 400	*0 U	40 U	40.0	41000	10 U	90	50.0	10 U	10 U	100	<b>10</b> U	50 U	50 0	40 U	100	100	10 U	100	90.0	40 II	40 U	140	100	300	Mo	NO U	90.0	900	40.0	≃00	70 U
VE SSI SU	09 HW 09	14.29	P	719 784	4700	100,00	1100	44000	10.0	50.9	10 U	NO U	*0 U	100	10 U	730	50 U	2800	100	70 U	10 U	400	40.0	20.0	*0 U	10 U	10 U	50 U	630/00	50 U	54	1600	19000		νου 1
																	Септион О	рильгия															_	=	
VE 25/24	15-14-4-06	1321	CUT	205 660	<b>40</b> U	1160	900	170000	-0 u	3C U	-0 U	40 U	<b>10 U</b>	<b>40 U</b>	<b>16</b> U	•0 U	50 U	1.70	493	10 U	MID	50 U	90 U	~0 U	10 U	730	<b>46 U</b>	N/U	170	50 U	50 V	50 U	30 U	33000	20
VE 25+24	15-Mov-OF	13.24	14	521 780	1400	9900	1200	430XC	100	40 U	~0 U	10 U	~0	*0 U	•n u	<b>10</b> U	40 U	2400	/90	*0 U	50 U	*0 U	40 U	~0 U	10 U	yn u	20 U	50 ()	42000D	50 U	10 U	1700	14000	7400	•au
VE 25/ 74	17 New 66	11 27	CUT	F11	10.	23	10	710	1.6	1.0	10	10	10	10	- 22	10	1.0	10	1 u	10	**	10	10	14	2 U	1.0	10	10	320	10	10	10	16	140	14
WE 25-24	17 New CO	11 26	14	450 340	1400	1200	1100	*9000	*0 U	50.0	50.0	*0 U	*C U	*0 U	-00	100	90 U	7300	740	NO U	10.0	-0 U	90.0	10 U	40 U	95.0	*0 U	40.0	250000	50 0	*0 U	1700	13000	400	*0 U
WE 25474 WE 2542N	27-40-04 27 WH CE	11.45	OUT	104 420	1900	12000	1300	94000 67000	50 U	40 u	90 U	*0 U	10 U	50 0	- VO U	63 70 U	90 u	1600	%0 U 520	10 U	49 U	<b>50</b> 0	40 U	40 U	*0 U	700	10 U	90 U	290000	10 U	53	₩0	11000	7000 7000	90
	44 -91 (4	11.51	JUI	114 4 751	.40	12500	-3101	-700b	-10	***		- 31	~ 0	-30	400	400	70	-169	2/4	-900	-00	30 U	-00	90	<b>₩</b> u	30	-0 U	50 U	37793	700	*0 U	1900		-600	-10

Charles D.F · De

Table 7-1 OPERATION SUMMARY AND ESTIMATED REMOVAL RATES FOR PILOT SVE SYSTEM OMEGA CHEMICAL SUPERFUND SITE

Date	System Status	Hours of Operation	Sample COLLECTED	Flow Rate (SCFM)	Flow Rate (SCFD)	Total VOC Conc. (ug/L)	PCE Conc. (ug/L)	Est. VOC Rem. Rate (lbs/day)	Est.PCE Rem. Rate (lbs/day)	Cum, VOC Removed (lbs)	Cum. PCE Removed (lbs)
17-Oct-06	On	5	1	56.86	81,878	280.60	151.98	1.42	0.77	0.3	0.2
18-Oct-06	On	12.5	2	55.00	79,200	1481.03	759.92	7.26	3.73	3	1
19-Oct-06	On	20	3	57.69	83,074	2439.95	1105.33	12.55	5.68	6	3
20-Oct-06	On	27	4	60.92	87,725	2627.01	1796.17	14.27	9.75	11	6
21-Oct-06	Off	27		0 00	0	0 00	0.00	0.00	0 00	11	6
22-Oct-06	Off	27		0 00	0	0 00	0.00	0.00	0 00 20.25	11	6 13
23-Oct-06	On	35.25 42.25	5 5	64.46 98.43	92.822 141,739	4369.10 1881.49	3523.25 1588.92	25.11 16.51	13.94	24	17
24-Oct-06 25-Oct-06	On On	47.25	7	103.36	148,838	2178.01	1450.75	20.07	13.37	28	20
26-Oct-06	On	54.25	8	86.72	124,877	4404.16	3108.75	34.05	24.03	38	27
27-Oct-06	On	61.25	ğ	82.27	118 469	4252.36	3523.25	31.19	25.84	47	34
28-Oct-06	. Off	61.25		0.00	0	0.00	0.00	00	0.0	47	34
29-Oct-06	Off	61 25		0.00	ō	0 00	0.00	00	0.0	47	34
30-Oct-06	On	68.25	10 ·	67.58	97,315	4577.23	4075.92	27.58	24.56	55	41
31-Oct-06	Off	68 25		0.00	0	0.00	0.00	0.0	0.0	55	41
1-Nov-06	On	74.25	11	64.46	92.822	3964.62	3246.92	22.78	18.66	61	46
2-Nov-06	On	80.75	12	178.58	257,155	2039.46	1796.17	32,47	28.59	70	54
3-Nov-06	On	87.25	13	185.06	266,486	2624.80	2072.50	43.30	34.19	82	63
4-Nov-06	Off	87.25		0 00	0	0 00	0 00	0 00	0 00	82	63
5-Nov-06	Off	87 25		0.00	0	0 00	0.00	0.0	0.0	82	63
6-Nov-06	Off	87.25	ا بد ا	0.00	0	0.00 3826.25	0.00	0.0	0 0 43.42	82 97	63 74
7-Nov-06	On On	93.25 99.25	14	176.27 170.47	253,829 245,477	5523.64	2763,33 4835.83	60.12 83.94	73.49	118	92
8-Nov-06 9-Nov-06	On On	105.25	15 16	124.74	179,626	4800,21	4352.25	53.38	48.40	131	104
10-Nov-06	Off	105.25	10	0 00	0	0 00	0.00	0.0	0.0	131	104
11-Nov-06	OH	105.25		0.00	0	0 00	0.00	0.0	0.0	131	104
12-Nov-06	Off	105.25		0.00	0	0.00	0.00	0.0	0.0	131	104
13-Nov-06	Off	105 25	1	0.00	ō	0.00	0.00	0.0	0.0	131	104
14-Nov-06	On	119.92		168.48	242,611	3386.99	2901.50	50.87	43.58	162	131
15 Nov-06	On	133.58	17	173.31	249.566	3386.99	2901.50	52.33	44.83	192	157
16-Nov-06	Off	133.58		0 00	0	0 00	0.00	0.0	0.0	192	157
17-Nav-06	On	148.58	18	180.33	259,675	3150.23	2694.25	50.64	43.31	223	184
18-Nov-06	On	172.58		180.33	259,675	2912.21	2495.29	47.31	40 54	271	224
19-Nov-06	On	196.58	' I	180.33	259,675	2674.20	2296.33	45 44	39.03	316	263
20-Nov-06	On	220.58		197.29	284,098	2436.18	2097.37	42.85	36.89	359	300
21-Nov-06	On	244.58		197.29	284,098	2198.16	1898 41	38.07	32.88	397	333
22-Nav-06	On Off	256.92 256.92	19	192.46 0.00	277,142 0	2075.85 0.00	1796.17	35.62	30.82 0.0	415 415	349 349
23-Nov-06 24-Nov-06	Off	256.92		0.00	0	0.00	0.00 0.00	0 0 0.0	0.0	415	349
24-Nov-06 25-Nov-06	Off	256.92 256.92		0.00	0	0.00	0.00	0.0	0.0	415	349
26-Nov-06	Off	256.92		0.00	0	0.00	0.00	0.0	0.0	415	349
27-Nov-06	Off	256.92		0.00	0	0.00	0.00	0.0	0.0	415	349
28-Nov-06	Off	256 92		0.00	ő	0 00	0.00	0.00	0.00	415	349
29-Nov-06	On	264.50	20	194.08	279.475	0.00	0.00	0.00	0.00	415	349
30-Nov-06	On	288.50	i	194.08	279,475	0.00	0.00	0.00	0.00	415	349
1-Dec-06	On	297.50		194 08	279,475	0.00	0.00	0.00	0 00	415	349
2-Dec-06	Off	297 50		0 00	0	0 00	0 00	0.00	0 00	415	349
3-Dec-06	Off	297.50		0.00	0	0 00	0.00	0.00	0.00	415	349
4-Dec-06	On	312.50		190.86	274,838	0 00	0.00	0.00	0.00	415	349
5-Dec-06	On	336.50		190.86	274,838	0.00	0.00	0.00	0.00	415	349
6-Dec-06	On O-	360.50		190 86	274,838	0.00	0.00	0.00	0.00	415	349
7-Dec-06 8-Dec-06	On Off	369.50 369.50		190.86 0 00	274,838 0	0.00 0.00	0.00 0.00	0 00	0.00	415 415	349 349
9-Dec-06	Off	369.50		0.00	0	0.00	0.00	0.00	0.00	415 415	349
10-Dec-06	Off	369.50		0.00	0	0.00	0.00	0.00	0.00	415	349
11-Dec-06	On	382.50		196.58	283,075	0.00	0.00	0.00	0.00	415	349
12-Dec-06	On	406.50		196.58	283.075	0 00	0.00	0.00	0.00	415	349
13-Dec-06	On	415.50		196.58	283,075	0.00	0.00	0.00	0.00	415	349
On	eration :	Summary	·:	209.9	7,254,878	3,062.1	2468	35.4	29.2	415	349
- 4		<b></b>		(avg.)	(total)	(avg.)	(avg.)	(avg.)	(avg.)	(total)	(total)
				(w·g.)	(cotal)	(4.8.)	(avg.)	(a v y./	(0.49.)	(total)	(total)